

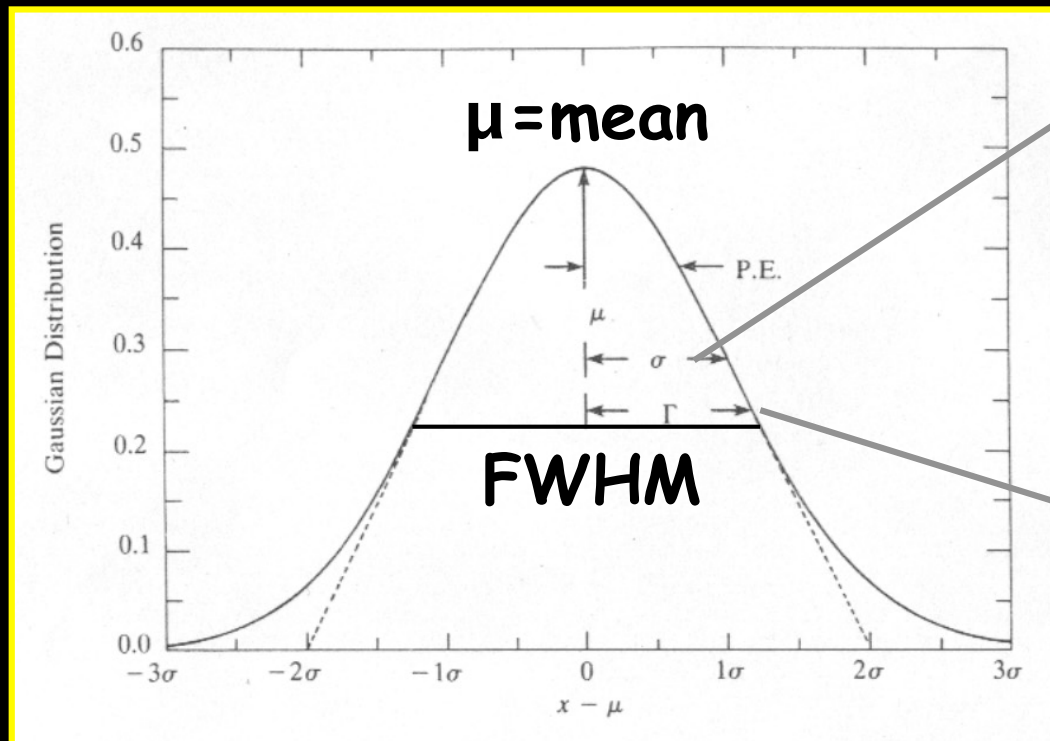
# *A taste of statistics and applications to X-ray spectral fitting*

- ✓ Normal error (Gaussian) distribution
  - most important in statistical analysis of data, describes the distribution of random observations for many experiments
- ✓ Poisson distribution
  - generally appropriate for counting experiments related to random processes (e.g., radioactive decay of elementary particles)
- ✓ Statistical tests:  $\chi^2$  and F-test

Further details in the XSPEC presentation

# The Gaussian (normal error) distribution

Casual errors are above and below the “true” (most “common”) value  
→ bell-shape distribution if systematic errors are negligible



$\sigma$  = standard deviation of the function

$\Gamma$  = half-width at half maximum =  $1.17\sigma$

$$\text{FWHM} = 2.35\sigma$$

## Gaussian probability function

$$P(x; \mu, \sigma) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{(x - \mu)^2}{2\sigma^2}}$$

*Probability Density  
Function*  
(centered on  $\mu$ )

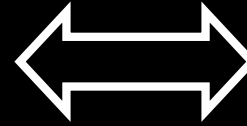
$\mu$ =mean value  
 $\sigma$ =standard deviation

normalization factor, so that  $\int f(x) dx=1$

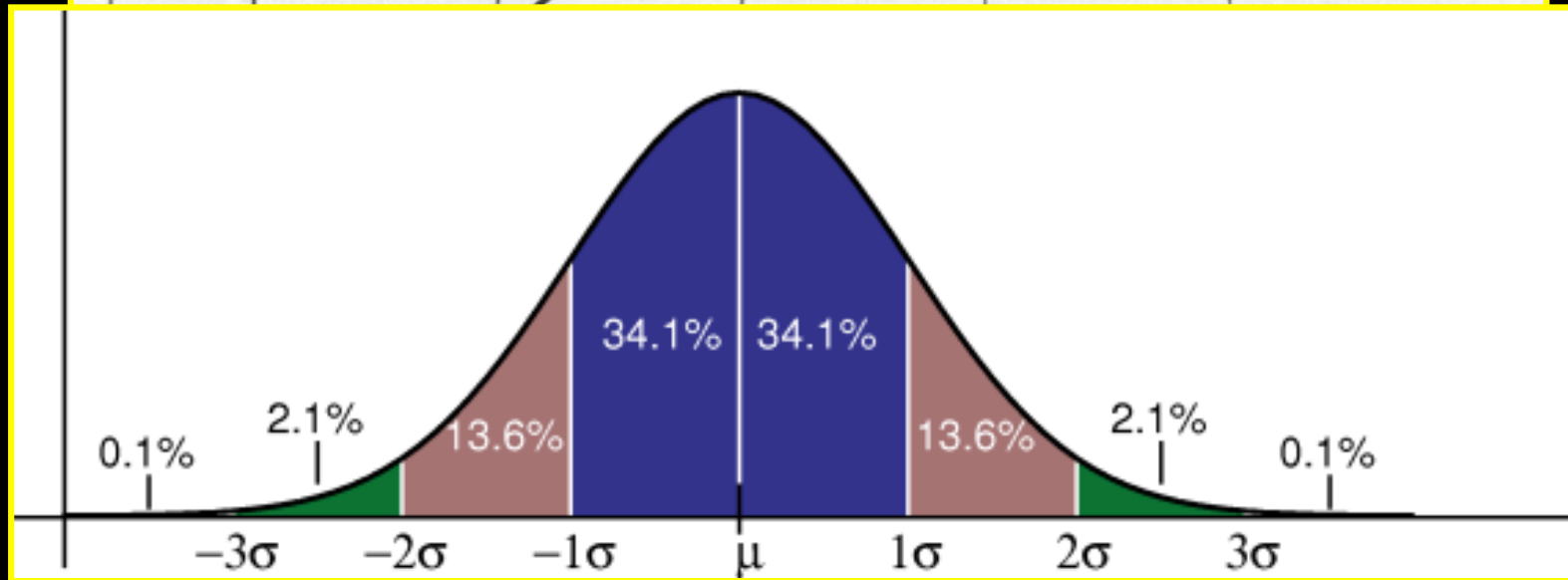
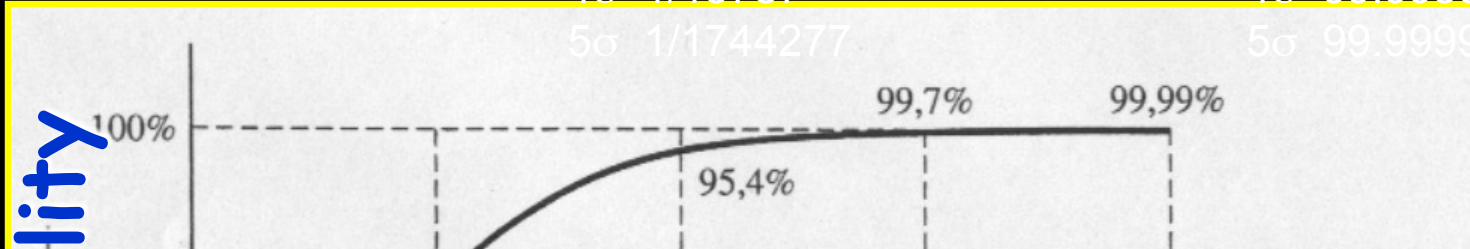
$$e^{-x^2 / 2\sigma^2}$$

function centered on 0

$1\sigma$  1/3  
 $2\sigma$  1/22  
 $3\sigma$  1/370  
 $4\sigma$  1/15787  
 $5\sigma$  1/1744277



$1\sigma$  68.3%  
 $2\sigma$  95.45%  
 $3\sigma$  99.730%  
 $4\sigma$  99.99367%  
 $5\sigma$  99.999943%



$\sigma$	0	0,25	0,5	0,75	1,0	1,25	1,5	1,75	2,0	2,5	3,0	3,5	4,0
P (%)	0	20	38	55	68	79	87	92	95,4	98,8	99,7	99,95	99,99

$$F(x) = \frac{1}{\sqrt{2\pi}\sigma} \int_{-\infty}^x e^{-(x-\mu)^2/2\sigma^2} dx$$

*Cumulative Distribution Function*

# The Poisson distribution

Describes experimental results where events are counted and the uncertainty is not related to the measurement but reflects the intrinsically casual behavior of the process (e.g., radioactive decay of particles, X-ray photons, etc.)

$$P(x) = e^{-\mu} \mu^x / x! \quad (x=0,1,2, \dots)$$

Probability of obtaining  $x$  events when the expected number is  $\mu$   
 $\mu > 0$ : main parameter of the Poisson distribution  
 $x$ =observed number of events in a time interval (frequency of events)

average  
number  
of events

$$\bar{x} = \sum_{x=0}^{\infty} xP(x) = \sum_{x=0}^{\infty} x e^{-\mu} \mu^x / x! = \mu$$

→  $\mu$ =average number of expected events if the experiment is repeated many times

$$\sigma^2 = \langle (x - \mu)^2 \rangle$$

expectation value of the square of the deviations

$$= \sum_{x=0}^{\infty} (x - \mu)^2 \frac{\mu^x}{x!} e^{-\mu} = \mu$$

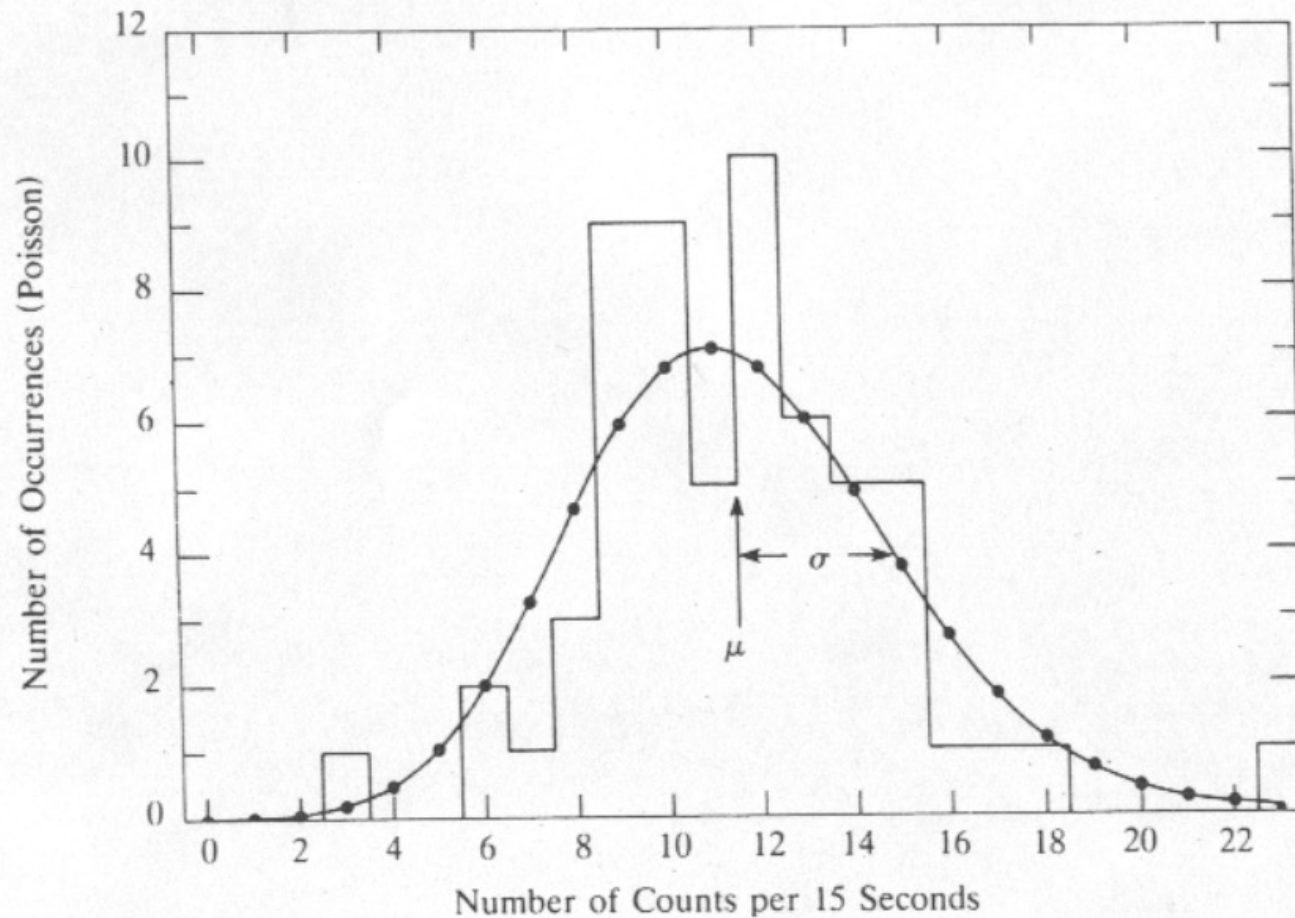


the Poisson distribution with average counts= $\mu$  has standard deviation  $\sqrt{\mu}$



$\mu \gg 1$  : the Poisson distribution is approximated by the Gaussian distribution

defined by only one parameter  $\mu$



# F-test

If two statistics following the  $\chi^2$  distribution have been determined, the ratio of the reduced chi-squares is distributed according to the F distribution

$$P_f(f; \nu_1, \nu_2) = \frac{\chi_1^2 / \nu_1}{\chi_2^2 / \nu_2}$$

$$\propto \Delta\chi^2 / k$$

with  $k$ =number of additional terms (parameters)

Example: Use the F-test to evaluate the improvement to a spectral fit due to the assumption of a different model, with additional terms

Conditions: (a) the simpler model is nested within the more complex model; (b) the extra parameters have Gaussian distribution (not truncated by the parameter space boundaries)

→ see the F-test tables for the corresponding probabilities (specific command in XSPEC)



# An application of the F-test

```

=====
Model phabs<1>*powerlaw<2> Source No.: 1 Active/On
Model Model Component Parameter Unit Value
par comp
 1 1 phabs nH 10^22 1.59000E-02 frozen
 2 2 powerlaw PhoIndex 2.72811 +/- 0.0
 3 2 powerlaw norm 1.51490E-04 +/- 0.0
    
```

Using energies from responses.

**Model1**

```

Chi-Squared = 97.23 using 105 PHA bins.
Reduced chi-squared = 0.9440 for 103 degrees of freedom
Null hypothesis probability = 6.417127e-01
    
```

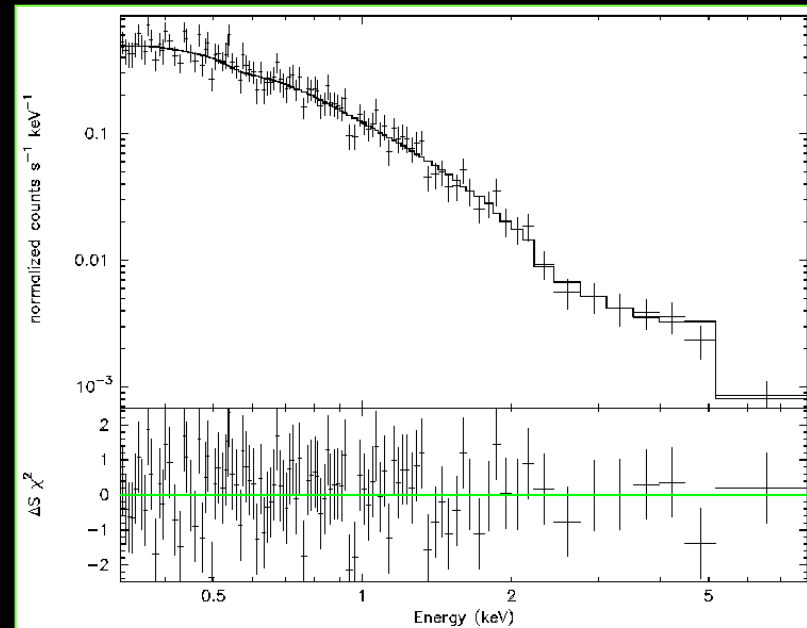
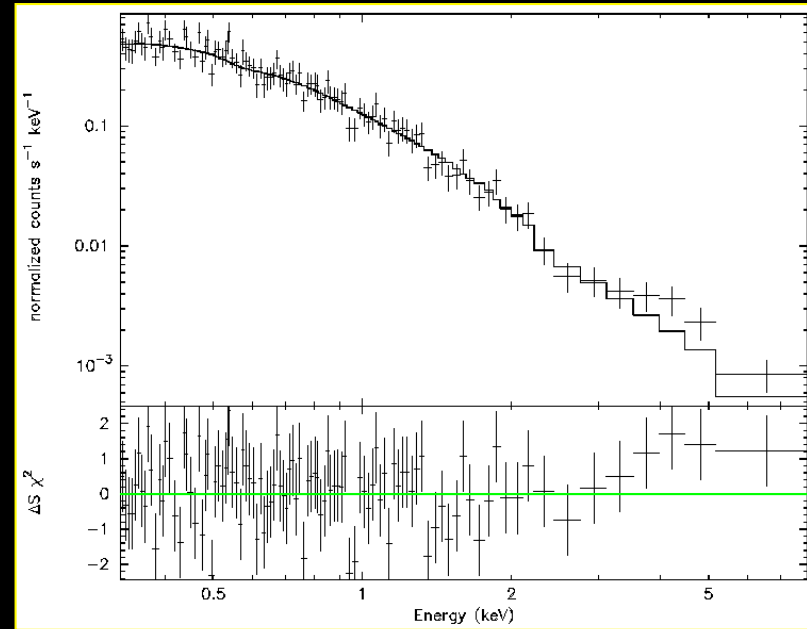
```

=====
Model phabs<1>(laor<2> + powerlaw<3>) Source No.: 1 Active/On
Model Model Component Parameter Unit Value
par comp
 1 1 phabs nH 10^22 1.59000E-02 frozen
 2 2 laor lineE keV 5.23582 +/- 0.0
 3 2 laor Index 3.00000 frozen
 4 2 laor Rin(G) 1.23500 frozen
 5 2 laor Rout(G) 400.000 frozen
 6 2 laor Incl deg 30.0000 frozen
 7 2 laor norm 6.83065E-06 +/- 0.0
 8 3 powerlaw PhoIndex 2.77137 +/- 0.0
 9 3 powerlaw norm 1.48123E-04 +/- 0.0
    
```

Using energies from responses. **Model1+extra component**

```

Chi-Squared = 90.84 using 105 PHA bins.
Reduced chi-squared = 0.8994 for 101 degrees of freedom
Null hypothesis probability = 7.557789e-01
Current data and model not fit yet. low F value => likely
Weighting method: standard low signif. of add. comp
XSPEC12> ftest 90.84 101 97.2 103
F statistic value = 3.53567 and probability 0.0327981
    
```



$$F_t = \left( \frac{\chi^2(dof) - \chi^2(dof - k)}{dof - (dof - k)} \right) / \left( \chi^2(dof - k) / (dof - k) \right) =$$

$$= (\Delta\chi^2/k) / \chi^2_\nu$$

$$\text{Ex: } \chi^2(103) = 97.23$$

$$\chi^2(101) = 90.84$$

$$\rightarrow \Delta\chi^2 = 6.39, k = 2 \rightarrow F_t = (6.39/2) / (90.84/101) = 3.55$$

$F_t$  follows the F distribution with  $v_1 = k = \Delta(\text{dof})$  and  $v_2 = \text{dof} - k(-1)$

➔ Search in the F-distribution tables for the probability of the null hypothesis ( $H_0$ ) for  $v_1 = 2$  and  $v_2 = 100$

$v_1=2$   
 $v_2=100$   
 (60-120)

$F=3.15, 3.07$   
 at  $P(F)=0.05$

$F=3.93, 3.80$   
 at  $P(F)=0.025$

$F_{xspec}=3.55$



Prob interm.  
 between 0.05  
 and 0.025  
 (actually,  
 0.0323)

TABLE 5 (Contd.)

$P(F) = 0.05$

$f_2 \backslash f_1$	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	$\infty$
1	161.45	199.50	215.71	224.58	230.16	233.99	236.77	238.88	240.54	241.88	243.91	245.95	248.01	249.05	250.09	251.14	252.20	253.25	254.32
2	18.51	19.00	19.16	19.25	19.30	19.33	19.35	19.37	19.38	19.40	19.41	19.43	19.45	19.45	19.46	19.47	19.48	19.49	19.50
3	10.13	9.55	9.28	9.12	9.01	8.94	8.89	8.85	8.81	8.79	8.74	8.70	8.66	8.64	8.62	8.59	8.57	8.55	8.53
4	7.71	6.94	6.59	6.39	6.26	6.16	6.09	6.04	6.00	5.96	5.91	5.86	5.80	5.77	5.75	5.72	5.69	5.66	5.63
5	6.61	5.79	5.41	5.19	5.05	4.95	4.88	4.82	4.77	4.74	4.68	4.62	4.56	4.53	4.50	4.46	4.43	4.40	4.36
6	5.99	5.14	4.76	4.53	4.39	4.28	4.21	4.15	4.10	4.06	4.00	3.94	3.87	3.84	3.81	3.77	3.74	3.70	3.67
7	5.59	4.74	4.35	4.12	3.97	3.87	3.79	3.73	3.68	3.64	3.57	3.51	3.44	3.41	3.38	3.34	3.30	3.27	3.23
8	5.32	4.46	4.07	3.84	3.69	3.58	3.50	3.44	3.39	3.35	3.28	3.22	3.15	3.12	3.08	3.04	3.01	2.97	2.93
9	5.12	4.26	3.86	3.63	3.48	3.37	3.29	3.23	3.18	3.14	3.07	3.01	2.94	2.90	2.86	2.83	2.79	2.75	2.71
10	4.96	4.10	3.71	3.48	3.33	3.22	3.14	3.07	3.02	2.98	2.91	2.84	2.77	2.74	2.70	2.66	2.62	2.58	2.54
11	4.84	3.98	3.59	3.36	3.20	3.09	3.01	2.95	2.90	2.85	2.79	2.72	2.65	2.61	2.57	2.53	2.49	2.45	2.40
12	4.75	3.89	3.49	3.26	3.11	3.00	2.91	2.85	2.80	2.75	2.69	2.62	2.54	2.51	2.47	2.43	2.38	2.34	2.30
13	4.67	3.81	3.41	3.18	3.03	2.92	2.83	2.77	2.71	2.67	2.60	2.53	2.46	2.42	2.38	2.34	2.30	2.25	2.21
14	4.60	3.74	3.34	3.11	2.96	2.85	2.76	2.70	2.65	2.60	2.53	2.46	2.39	2.35	2.31	2.27	2.22	2.18	2.13
15	4.54	3.68	3.29	3.06	2.90	2.79	2.71	2.64	2.59	2.54	2.48	2.40	2.33	2.29	2.25	2.20	2.16	2.11	2.07
16	4.49	3.63	3.24	3.01	2.85	2.74	2.66	2.59	2.54	2.49	2.42	2.35	2.28	2.24	2.19	2.15	2.11	2.06	2.01
17	4.45	3.59	3.20	2.96	2.81	2.70	2.61	2.55	2.49	2.45	2.38	2.31	2.23	2.19	2.15	2.10	2.06	2.01	1.96
18	4.41	3.55	3.16	2.93	2.77	2.66	2.58	2.51	2.46	2.41	2.34	2.27	2.19	2.15	2.11	2.06	2.02	1.97	1.92
19	4.38	3.52	3.13	2.90	2.74	2.63	2.54	2.48	2.42	2.38	2.31	2.23	2.16	2.11	2.07	2.03	1.98	1.93	1.88
20	4.35	3.49	3.10	2.87	2.71	2.60	2.51	2.45	2.39	2.35	2.28	2.20	2.12	2.08	2.04	1.99	1.95	1.90	1.84
21	4.32	3.47	3.07	2.84	2.68	2.57	2.49	2.42	2.37	2.32	2.25	2.18	2.10	2.05	2.01	1.96	1.92	1.87	1.81
22	4.30	3.44	3.05	2.82	2.66	2.55	2.46	2.40	2.34	2.30	2.23	2.15	2.07	2.02	1.98	1.94	1.89	1.84	1.78
23	4.28	3.42	3.03	2.80	2.64	2.53	2.44	2.37	2.32	2.27	2.20	2.13	2.05	2.00	1.96	1.91	1.86	1.81	1.76
24	4.26	3.40	3.01	2.78	2.62	2.51	2.42	2.36	2.30	2.25	2.18	2.11	2.03	1.98	1.94	1.89	1.84	1.79	1.73
25	4.24	3.39	2.99	2.76	2.60	2.49	2.40	2.34	2.28	2.24	2.16	2.09	2.01	1.96	1.92	1.87	1.82	1.77	1.71
26	4.23	3.37	2.98	2.74	2.59	2.47	2.39	2.32	2.27	2.22	2.15	2.07	1.99	1.95	1.90	1.85	1.80	1.75	1.69
27	4.21	3.35	2.96	2.73	2.57	2.46	2.37	2.31	2.25	2.20	2.13	2.06	1.97	1.93	1.88	1.84	1.79	1.73	1.67
28	4.20	3.34	2.95	2.71	2.56	2.45	2.36	2.29	2.24	2.19	2.12	2.04	1.96	1.91	1.87	1.82	1.77	1.71	1.65
29	4.18	3.33	2.93	2.70	2.55	2.43	2.35	2.28	2.22	2.18	2.10	2.03	1.94	1.90	1.85	1.81	1.75	1.70	1.64
30	4.17	3.32	2.92	2.69	2.53	2.42	2.33	2.27	2.21	2.16	2.09	2.01	1.93	1.89	1.84	1.79	1.74	1.68	1.62
60	4.08	3.28	2.84	2.61	2.45	2.34	2.25	2.18	2.12	2.08	2.00	1.92	1.84	1.79	1.74	1.69	1.64	1.58	1.51
120	4.00	3.15	2.76	2.53	2.37	2.25	2.17	2.10	2.04	1.99	1.92	1.84	1.75	1.70	1.65	1.59	1.53	1.47	1.39
$\infty$	3.84	3.00	2.60	2.37	2.21	2.10	2.01	1.94	1.88	1.83	1.75	1.67	1.57	1.52	1.46	1.39	1.32	1.22	1.00

$P(F)=0.05$

$P(F) = 0.025$

$f_2 \backslash f_1$	1	2	3	4	5	6	7	8	9	10	12	15	20	24	30	40	60	120	$\infty$
1	647.79	799.50	864.16	899.58	921.85	937.11	948.22	956.66	963.28	968.63	976.71	984.87	993.10	997.25	1001.4	1005.6	1009.8	1014.0	1018.3
2	38.51	39.00	39.16	39.25	39.30	39.33	39.36	39.37	39.39	39.40	39.42	39.43	39.45	39.46	39.46	39.47	39.48	39.49	39.50
3	17.44	16.04	15.44	15.10	14.88	14.74	14.62	14.54	14.47	14.42	14.34	14.25	14.17	14.12	14.08	14.04	13.99	13.95	13.90
4	12.22	10.65	9.98	9.60	9.36	9.20	9.07	8.98	8.90	8.84	8.75	8.66	8.56	8.51	8.46	8.41	8.36	8.31	8.26
5	10.01	8.43	7.76	7.39	7.15	6.98	6.85	6.76	6.68	6.62	6.52	6.43	6.33	6.28	6.23	6.18	6.12	6.07	6.02
6	8.81	7.26	6.60	6.23	5.99	5.82	5.70	5.60	5.52	5.46	5.37	5.27	5.17	5.12	5.07	5.01	4.96	4.90	4.85
7	8.07	6.54	5.89	5.52	5.29	5.12	4.99	4.90	4.82	4.76	4.67	4.57	4.47	4.42	4.36	4.31	4.25	4.20	4.14
8	7.57	6.06	5.42	5.05	4.82	4.65	4.53	4.43	4.36	4.30	4.20	4.10	4.00	3.95	3.89	3.84	3.78	3.73	3.67
9	7.21	5.71	5.08	4.72	4.48	4.32	4.20	4.10	4.03	3.96	3.87	3.77	3.67	3.61	3.56	3.51	3.45	3.39	3.33
10	6.94	5.46	4.83	4.47	4.24	4.07	3.95	3.85	3.78	3.72	3.62	3.52	3.42	3.37	3.31	3.26	3.20	3.14	3.08
11	6.72	5.26	4.63	4.28	4.04	3.88	3.76	3.66	3.59	3.53	3.43	3.33	3.23	3.17	3.12	3.06	3.00	2.94	2.88
12	6.55	5.10	4.47	4.12	3.89	3.73	3.61	3.51	3.44	3.37	3.28	3.18	3.07	3.02	2.96	2.91	2.85	2.79	2.72
13	6.41	4.97	4.35	4.00	3.77	3.60	3.48	3.39	3.31	3.25	3.15	3.05	2.95	2.84	2.79	2.73	2.67	2.61	2.55
14	6.30	4.86	4.24	3.89	3.66	3.50	3.38	3.29	3.21	3.15	3.06	2.96	2.86	2.76	2.70	2.64	2.58	2.52	2.46
15	6.20	4.76	4.15	3.80	3.58	3.41	3.29	3.20	3.12	3.06	2.96	2.86	2.76	2.66	2.60	2.54	2.48	2.42	2.36
16	6.12	4.69	4.08	3.73	3.50	3.34	3.22	3.12	3.05	2.99	2.89	2.79	2.68	2.63	2.57	2.51	2.45	2.38	2.32
17	6.04	4.62	4.01	3.66	3.44	3.28	3.16	3.06	2.98	2.92	2.82	2.72	2.62	2.56	2.50	2.44	2.38	2.32	2.25
18	5.98	4.56	3.95	3.61	3.38	3.22	3.10	3.01	2.93	2.87	2.77	2.67	2.56	2.50	2.44	2.38	2.32	2.26	2.19
19	5.92	4.51	3.90	3.56	3.33	3.17	3.05	2.96	2.88	2.82	2.72	2.62	2.51	2.45	2.39	2.33	2.27	2.20	2.13
20	5.87	4.46	3.86	3.51	3.29	3.13	3.01	2.91	2.84	2.77	2.68	2.57	2.46	2.41	2.35	2.29	2.22	2.16	2.09
21	5.83	4.42	3.82	3.48	3.25	3.09	2.97	2.87	2.80	2.73	2.64	2.53	2.42	2.37	2.31	2.25	2.18	2.11	2.04
22	5.79	4.38	3.78	3.44	3.22	3.05	2.93	2.84	2.76	2.70	2.60	2.50	2.39	2.33	2.27	2.21	2.14	2.08	2.00
23	5.75	4.35	3.75	3.41	3.18	3.02	2.90	2.81	2.73	2.67	2.57	2.47	2.36	2.30	2.24	2.18	2.11	2.04	1.97
24	5.72	4.32	3.72	3.38	3.15	2.99	2.87	2.78	2.70	2.64	2.54	2.44	2.33	2.27	2.21	2.15	2.08	2.01	1.94
25	5.69	4.29	3.69	3.35	3.13	2.97	2.85	2.75	2.68	2.61	2.51	2.41	2.30	2.24	2.18	2.12	2.05	1.98	1.91
26	5.66	4.27	3.67	3.33	3.10	2.94	2.82	2.73	2.65	2.59	2.49	2.39	2.28	2.22	2.16	2.09	2.03	1.95	1.88
27	5.63	4.24	3.65	3.31	3.08	2.92	2.80	2.71	2.63	2.57	2.47	2.36	2.25	2.19	2.13	2.07	2.00	1.93	1.85
28	5.61	4.22	3.63	3.29	3.06	2.90	2.78	2.69	2.61	2.55	2.45	2.34	2.23	2.17	2.11	2.05	1.98	1.91	1.83
29	5.59	4.20	3.61	3.27															